

ASX Announcement 27 February 2023

Catalina Resources is an Australian diversified mineral exploration and mine development company.

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REE and lithium mineralisation discovered in air core drilling at Dundas

Catalina Resources ("Catalina" or "the Company") is pleased to provide details of the initial and recently completed air core drilling program at Dundas project.

Highlights

- First assays from the maiden air core drilling program at Dundas confirm grades up to 0.81% (8146 ppm) total rare earth element oxides (TREO), including 0.16% Nd₂O₃, in hole 22DAC095.
- Another hole (22DAC066) intersected 0.65% TREO, including 0.12% Nd₂O₃ and 0.14% La₂O₃, with coincident anomalous lithium geochemistry.
- Lithium averaging 84 ppm over 44m to the end of hole (EOH) and 103 ppm over 28m to EOH has also been intersected. Anomalous REE assays also accompany the lithium.
- The anomalous drilling geochemistry occurs within deeply oxidised regolith and saprolite (clay) zones. It has developed by in-situ weathering of an unknown bedrock.
- Anomalous REE mineralisation also occurs in bedrock in several holes below the regolith horizons. Excellent potential exists for higher grade, higher commercial value, hard rock REE mineralisation in the project area.
- Assays confirm a critical heavy rare earth oxide (HREO) ratio NdPr+DyTb of 19% of total REEs.
- The assays are derived from 4m composite samples, and it is expected that dilutionary effects of this sampling has reduced grades of mineralisation.
- Increased grades are expected from the individual one metre sampling intervals that make up the 4m composite samples.

A 105-hole air core drill program was completed at the Dundas Project in December 2022 for a total of 2909m with an average depth of 27.7m. Air core drilling is done to blade refusal (rock too hard to penetrate). The Dundas Project occurs in a green fields' region in the Albany Fraser Belt of WA. Its regional location is shown in Figure 1.

These very anomalous REE and lithium assays puts Dundas project on the path of a significant REE and lithium discovery in a highly prospective and very underexplored location. Assays indicate significant REE intersections up to 16m thick and anomalous lithium intersections up to 44m thick are present. The coincidence of lithium with the anomalous REE geochemistry is unusual and reiterates the prospectivity of the region.

A 6-20m blanket of transported colluvium and lake clays overlies and masks the bedrock geology. To look below this blanket air core drilling

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successfully intersected geochemical and lithological information of the bedrock to plan follow up RC drilling. Essentially the air core work has identified the geochemical halo to a potentially larger target at depth. Deeper RC drilling will be planned to drill underneath and along strike of these air core anomalies.

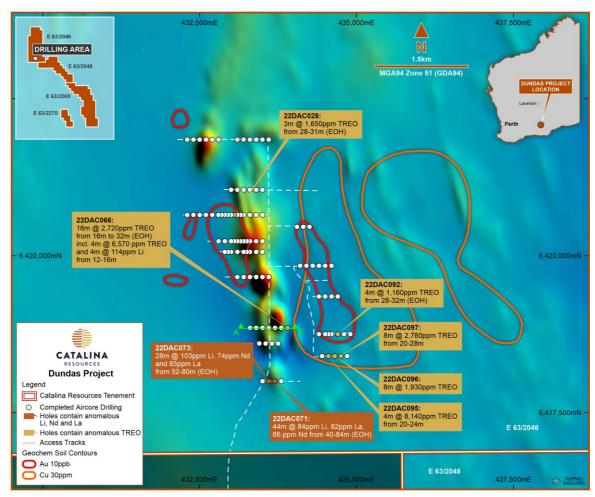


Figure 1. Air core drilling and assay summary. Underlying image is the regional aeromagnetic image.

Significant REE intersections include:

- 16m @ 2720 ppm TREO from 16 32m (EOH) in hole 22DAC066, including.
 - 4m @ 6570 ppm TREO from 16-20m, including 1270 ppm Nd_2O_3 , 135 ppm Dy_2O_3 .
 - 4m @ 114 ppm Li from 12-16m
- o 4m @ 8140 ppm TREO from 20 24m in hole 22DAC095, including.
 - 4m @ 1586 ppm Nd₂O₃, 1419 ppm La₂O₃, 3,536 ppm CeO₂ from 20-24m.
- o 8m @ 2790 ppm TREO from 20 28m in hole 22DAC097.

Significant lithium intersections include:

- o 4m @ 114 ppm Li from 12-16m in hole 22DAC066.
- o 44m @ 84 ppm Li, 82 ppm La, 66 ppm Nd from 40 -84m (EOH) in hole 22DAC071
- o 28m @ 103 ppm Li, 74 ppm Nd, 85 ppm La from 52 80m (EOH) in hole 22DAC073





The assays display an 'exceptional' heavy rare earth oxide (HREO) ratio of 19% of NdPr+DyTb to total TREOs. These four REEs are valuable and are rare magnet metals. The most powerful electric motor magnets used today are known as permanent magnets because they maintain their magnetic properties. They typically are made of neodymium iron boron (NdFeB). Dysprosium (Dy) and praseodymium (Pr) are also commonly used in permanent magnets. The growth in NdFeB magnets is attributed to increased use in the automotive industry and electric vehicle drivetrains. Local companies mining for NdPr is Lynas Rare Earth mine at Mt Weld in the Eastern Goldfields of WA.

Regolith and bedrock enrichments.

Significant REE enrichment in the regolith at Dundas is the result of weathering induced clay formation and REEs can be either enriched or depleted in different depth horizons of the regolith. Of note is the presence of anomalous REE mineralisation in bedrock in several holes below the regolith horizons. This suggests potential exists at Dundas for higher grade, higher commercial value, hard rock REE mineralisation. For example, figure 2 illustrates the laid-out air core samples for hole 22DAC066. The last 4m composite sample assayed 1386 ppm TREO at the end of hole. The sample has been logged as an amphibolite and illustrates that significant REE mineralisation in fresh rock is present at Dundas.

Figure 3 illustrates drilling cross-section A-A'. Its location is shown in figure 1. Mineralisation is either restricted to the regolith in hole 22DAC063 or can extend into the fresh rock, as discussed above for hole 22DAC066.



Figure 2. Laid-out **s**ample piles for air core hole 22DAC066. Significant REE geochemistry extends to the fresh rock at the end of hole. It is an important observation, suggesting that higher grade, hard rock mineralisation is present at Dundas.



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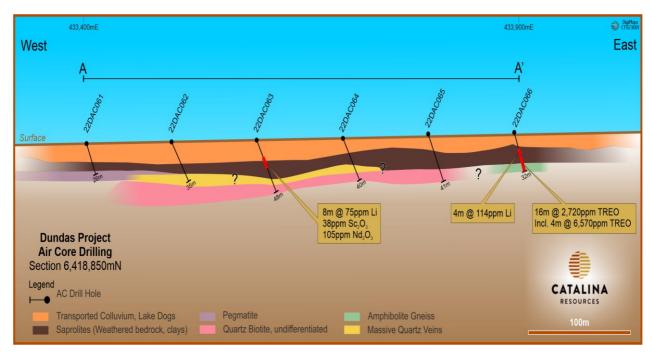


Figure 3. Drilling cross-section, A-A'.

Anomalous lithium was received in several air core holes, illustrated in figure 1. Lithium averaging 84 ppm over 44m to the end of hole (EOH) in 22DAC071 and 103 ppm over 28m to EOH in 22DAC073 is also accompanied by anomalous REE assays, including Nd and La. Holes were logged as thick intervals of graphitic, sometimes pyritic, siltstones and greywackes.

Air core drilling did not extend deep enough to explain the lithium occurrences in these holes. Several pegmatite bodies were logged in other holes (as in figure 3).

All REE assays for TREO contents > 500 ppm are in appendix 1. Collar coordinates for all drilling is in appendix 2.

Next Steps.

The collection of the 1m re-splits of the anomalous 4m composite samples, re-logging of lithologies, followed by RC drilling underneath and along strike of the air core targets.

As the project is in the Dundas National Park, additional tenement conditions over and above that for normal exploration licences are in force. These tenement conditions include Prior to any environmental disturbance, the licensee preparing a detailed CMP (Conservation Management Plan) for each phase of proposed exploration for approval. The Minister for Environment and the Conservation and Parks Commission has formal requirements under Section 24 of the Mining Act 1978 (Mining Act) to provide formal recommendations on proposed activities in Dundas Nature Reserve prior to the Minister for Mines and Petroleum providing his consent. DBCA reviews and presents the information prepared by and on behalf of the applicant (including copies of the proposal document(s)) to the Minister for Environment and the Conservation and Parks Commission in the form of a Conservation Management Plan (CMP).

A new CMP has been developed and lodged with the DBCA in November 2022 for the next phase of exploration including deeper drilling. This CMP was updated and lodged in February 2023 following a meeting with DBCA and feedback received on the November draft version.

Catalina expects to begin deeper drilling, via RC methods, in a few months once the above processes are completed and approved and subject to weather conditions as Catalina has made commitments that exploration activities will not be conducted under high fire risk conditions or when local fire bans have been



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declared and to access the reserve only during dry soil conditions as accessing of Dundas Nature Reserve during the wet season may risk the rutting and erosion of tracks.

ABOUT DUNDAS PROJECT

The Dundas project is in the Dundas Nature Reserve located approximately 90 km southeast of Norseman (Figure 4).

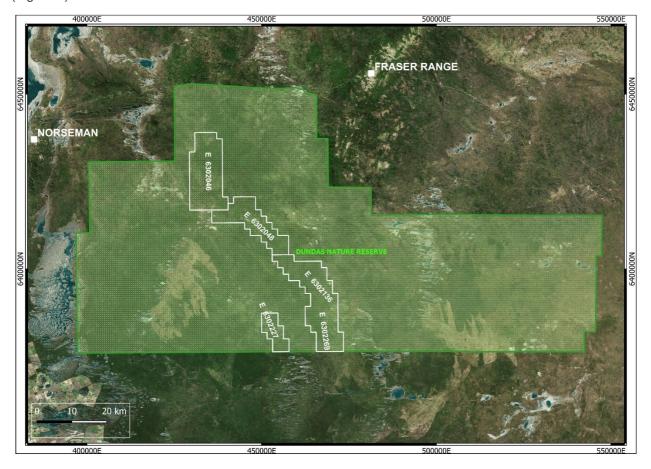


Figure 4 Location of Catalina Resources' Tenements within the Dundas Nature Reserve

The Dundas Project area is situated within the inferred SE extensions of the mineralised Norseman – Wiluna Belt of the Archaean Yilgarn Craton and comprises a tectonostratigraphic assemblage of mafic, ultramafic and sedimentary dominated units. A major northwest trending fault system transects the tenements and may represent the prospective Boulder-Lefroy Fault Zone (BLFZ) and the Zuleika Shear Systems (ZS), illustrated in figure 5. These shears and faults are highly prospective for gold (Swager et al., 1995). The tenements are also prospective for lithium mineralisation being only 25 kms to the southwest of Liontown's Buldania Lithium Project, also along the Zuleika Shear Zone, figure 5. Field work and historical reporting has confirmed the presence of pegmatites within the tenements.



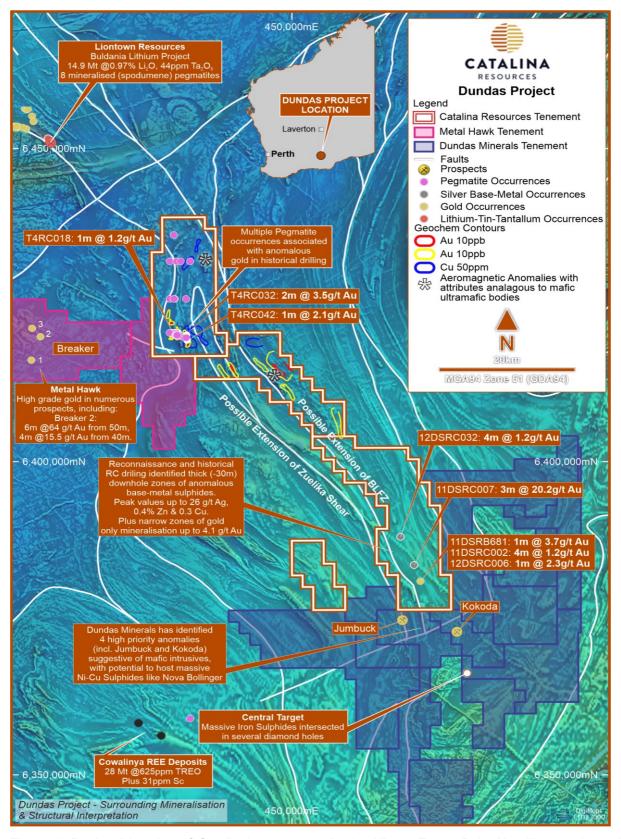


Figure 4. Regional location of Catalina's tenements in the Albany Fraser Belt. Also illustrated are the projects and highlights of respected neighbouring companies including Metal Hawk and Dundas Minerals.



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Competent Person Statement

The review of historical exploration activities and results contained in this report is based on information compiled by Michael Busbridge, a Member of the Australian Institute of Geoscientists, and a Member of the Society of Economic Geologists. He is a Director of Catalina Resources Ltd. He has sufficient experience which is relevant to the style of mineralisation and types of deposits under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (the JORC Code).

Michael Busbridge has consented to the inclusion in the report of the matters based on his information in the form and context in which it appears.

The Company confirms that it is not aware of any new information or data that materially affects the information in the original reports, and that the form and context in which the Competent Person's findings are presented have not been materially modified from the original reports.

The release of this document to the market has been authorised by the Board of Catalina Resources Ltd

ABOUT CATALINA RESOURCES LTD

Catalina Resources Ltd is an Australian diversified mineral exploration and mine development company whose vision is to create shareholder value through the successful exploration of prospective gold, base metal, lithium, REEs and iron ore projects and the development of these projects into production. The company's portfolio of tenements are located in highly prospective terrains in NSW (Lachlan Fold Belt) and WA (Eastern Goldfields and Albany Fraser Belt).



APPENDIX 1: AIR CORE DRILL ASSAYS > 500 PPM TREO

Holo Id	Depth	Depth																				TREO	HREO	HREO/
Hole_ld	From	To	Ве	CeO2	Dy ₂ O ₃	Er ₂ O ₃	Eu ₂ O ₃	Gd_2O_3	Ho ₂ O ₃	La ₂ O ₃	Li	Lu ₂ O ₃	Nd ₂ O ₃	Ni	Pr ₆ O ₁₁	Sc ₂ O ₃	Sm ₂ O ₃	Tb ₂ O ₃	Tm ₂ O ₃	Y_2O_3	Yb_2O_3	ppm	ppm	TREO
22DAC095	20	24	3.5	3537	116	41	58	194	18	1419	11.50	3	1586	54	414	21	256	24	4	428	27	8147	913	11%
22DAC066	16.00	20.00	21	2849	135	60	57	213	23	741	32.00	6	1271	182	300	28	238	26	7	568	47	6571	1144	17%
22DAC097	24	28	15	1424	50	23	22	76	9	438	18.50	2	499	202	138	12	95	9	3	305	18	3124	518	17%
22DAC097	20	24	15	1033	39	21	16	56	8	406	12.50	2	394	206	113	12	70	7	2	249	16	2444	416	17%
22DAC096	24	28	7.5	914	32	15	15	51	6	249	24.00	1	344	126	83	12	65	6	2	184	11	1991	325	16%
22DAC096	20	24	30	640	45	26	12	54	10	286	10.00	3	257	370	66	6	48	8	3	391	20	1874	571	30%
22DAC066	20.00	24.00	5	720	32	15	15	56	6	235	34.00	1	324	86	80	28	63	7	2	130	11	1724	275	16%
22DAC028	28	31	1	907	10	3	8	21	1	249	3.50	0	268	6	73	31	43	2	0	31	2	1650	79	5%
22DAC066	28.00	32.00	4	589	26	10	12	43	4	195	17.00	1	271	48	65	15	51	5	1	90	8	1386	200	14%
22DAC066	24.00	28.00	3	473	23	9		39	4	176	34.00	1	260	66	62	15	46	5	1	81	7	1213	181	15%
22DAC092	28	32	1.5	517	5	2		12		332	2.50	0	168	8	53	9	23	1	0		2	1159	57	5%
22DAC061B	8.00	12.00	3.5	415	19	10	8	29	4	201	21.50	1	183	254	46	21	34	4	1	132	8	1115	215	19%
22DAC093	44	47	1	436	17	6				145	8.50	1	222	36	54	58	45			59	5	1096	135	12%
22DAC011	16.00	20.00	1	497	11	4		18		202	6.50	0		46	47	18	30	_		43	3	1061	91	9%
22DAC090	20	24	1	486	11	4		21	2	190	21.00	0	162	90	41	40	31	2		37	3	1037	87	8%
22DAC001	32.00	36.00	0.5		19	8		34	3	236	9.50	1	255	66	64	25	46			86	6	1007	173	17%
22DAC027	28	29	1.5		14	5		24	2	163	6.00	0	.00	6	41	15	31	3		47	3	1001	105	11%
22DAC063	8.00	12.00	4	403	10	5		17		188	28.50	1	167	252	46	21	26			53	4	952	101	11%
22DAC095	32	36	1.5		12	5			2	149	8.50	1	177	32	47	18	32	_		43	4	952	97	10%
22DAC047	20	24	0.5		7	3				219	44.00			128	44	25	26	2	0	28	2	927	64	7%
22DAC001	36.00	40.00	1	333	17	7		25		148	6.50	1	176	90	44	25	33	3	1	79	6	907	149	16%
22DAC001	36.00	40.00	1	335	17	7	- ·	25		145	6.50	1	177	86	44	21	34	3		78	6	905	148	16%
22DAC066	12.00	16.00	13		12	9				35	114.00	1	53	614	13	18	12	_		91	8	901	143	16%
22DAC060	28	32	2	300	14	7	- ·			156	18.00	1	195	44	49	18	34	3		78	6	896	143	16%
22DAC095	36	37	1.5		21	8				161	22.00	1	136	126	33	25	28	4		85	7	867	170	20%
22DAC090	20	24	1	372	9	3		18	1	162	20.50			88	36	37	27	2			2	851	78	9%
22DAC094	20	24	2		5	2		9		191	14.50			46	38	21	17	1	0	17	2	844	40	5%
22DAC026	24	28	1	271	11	5				190	7.50			12	45	18	29			57	4	832	108	13%
22DAC077	16.00	20.00	1	441	5	2		10	1	162	6.00	0		14	31	15	17		0		2	830	53	6%
22DAC016	24	28	1.5		7	2		14	1	147	21.50	0	.00	68	42	40	27	2		20	2	829	52	6%
22DAC094	24	26	1.5		5	2		10		150	12.50	0		36	41	21	21	1	0	16	2	808	41	5%
22DAC061	16.00	20.00	2	433	7	3			<u> </u>	138	20.50	0		84	26	25	14	1	0	34	3	788	62	8%
22DAC092	24	28	1.5	307	5	2	4	10	1	228	7.50	0	129	26	40	9	18	1	0	25	2	781	50	6%



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Hole_ld	Depth From	Depth To	Be	CeO₂	Dy ₂ O ₃	Er₂O₃	Eu ₂ O ₃	Gd₂O₃	Ho ₂ O ₃	La₂O₃	Li	Lu₂O₃	Nd ₂ O ₃	Ni	Pr ₆ O ₁₁	Sc ₂ O ₃	Sm₂O₃	Tb ₂ O ₃	Tm ₂ O ₃	Y ₂ O ₃	Yb_2O_3	TREO ppm	HREO ppm	HREO/ TREO
22DAC094	0	4	2	303	13	6	6	19	2	116	29.50	1	138	70	35	18	26	2	1	63	5	754	117	16%
22DAC061A	8.00	12.00	4.5	266	14	8	6	20	3	123	28.00	1	121	232	31	28	23	3	1	96	6	750	157	21%
22DAC092	24	28	2	295	5	2	3	10	1	215	7.00	0	122	28	38	9	18	1	0	23	2	744	48	6%
22DAC036	24	28	2.5	282	9	4	5	15	2	127	25.50	1	143	78	38	43	24	2	1	42	4	741	83	11%
22DAC036	24	28	2.5	271	9	5	5	15	2	135	26.00	1	139	82	37	43	23	2	1	44	4	734	85	12%
22DAC090	20	26	1.5	329	4	2	2	6	1	251	14.50	0	52	56	20	34	7	1	0	18	1	727	34	5%
22DAC040	16	20	1	305	5	2	3	8	1	219	13.50	0		64	28	25	13	1	0	20	2	713	41	6%
22DAC065	32.00	36.00	2	189	8	3	6	15	1	178	33.00	0	159	102	43	34	25	2	0	35	3	703	75	11%
22DAC062	8.00	12.00	4.5	249	13	7	5	17	3	126	31.00	1	112	162	30	15	19	2	1	96	6	701	150	21%
22DAC060	20	24	1	131	6	2	4	11	1	305	23.50	0	120	54	45	15	16	1	0	28	2	688	55	8%
22DAC060	16	20	1.5	87	5	2	3	9	1	369	27.50	0	108	70	43	18	13	1	0	21	1	682	43	6%
22DAC001	40.00	41.00	1.5	230	15	7	6	21	3	105	4.50	1	125	36	29	21	24	3	1	77	6	672	139	21%
22DAC076	24.00	25.00	2	319	5	2	4	10	1	133	2.50	0	93	6	26	25	16	1	0	19	2	656	44	7%
22DAC040	16	20	1	280	5	2	2	8	1	201	12.50	0	76	60	26	21	12	1	0	19	1	655	39	6%
22DAC073	52.00	56.00	4	278	14	8	2	15	3	91	102.00	1	92	34	26	21	17	2	1	75	7	653	128	20%
22DAC092	20	24	1.5	287	4	2	3	8	1	162	5.00	0	103	16	31	9	15	1	0	20	2	647	41	6%
22DAC074	44.00	48.00	4	274	13	7	3	15	2	92	90.00	1	90	48	25	21	17	2	1	70	6	639	120	19%
22DAC071	76.00	80.00	4.5	273	13	7	2	15	2	96	86.50	1	94	34	27	18	17	2	1	63	6	638	113	18%
22DAC072	4.00	8.00	3	221	13	8	4	17	3	107	33.00	1	103	128	27	18	19	2	1	87	6	637	142	22%
22DAC027	24	28	1	254	7	3	4	12	1	135	15.00	0	114	36	31	25	20	1	0	27	2	636	58	9%
22DAC073	44.00	48.00	4.5	263	13	7	2	15	2	92	74.50	1	94	34	26	21	18	2	1	67	6	632	118	19%
22DAC073	40.00	44.00	4.5	254	14	8	2	16	3	90	73.00	1	92	34	25	21	18	2		74	7	630	129	21%
22DAC073	68.00	72.00	4	269	13	7	3	15	2	90	103.00	1	87	44	24	21	16	2	1	70	6	629	121	19%
22DAC073	60.00	64.00	4	262	13	7	2	14	2	90	95.00	1	88	34	24	21	17	2	1	70	6	622	120	19%
22DAC073	48.00	52.00	4.5	265	13	7	2	15	2	89	86.00	1	91	36	25	21	18	2	1	63	6	622	113	18%
22DAC073	32.00	36.00	4.5	259	13	7	2	15	2	89	72.50	1	92	36	25	21	17	2	1	63	6	616	113	18%
22DAC075	32.00	36.00	2	270	6	3	4	12	1	90	11.50	0	109	34	28	40	20	1	0	28	2	614	58	9%
22DAC071	80.00	84.00	4.5	259	12	6	2	14	2	92	82.50	1	92	34	26	18	17	2	1	61	6	612	108	18%
22DAC073	36.00	40.00	4.5	262	12	7	2	14	2	93	70.50	1	90	34	25	18	16	2	1	60	6	612	107	17%
22DAC037	16	17	1.5	303	3	2	2	5	1	154	10.00	0	67	26	26	21	8	1	0	16	2	610	31	5%
22DAC073	56.00	60.00	3.5	260	12	6	2	14	2	85	110.00	1	82	56	23	21	15	2	1	61	6	594	106	18%
22DAC002	36.00	40.00	1.5	282	4	2	3	8	1	123	6.00	0	91	26	27	21	14	1	0	15	1	593	34	6%
22DAC059	40.00	44.00	1.5	278	7	3	4	12	1	80	22.00	0	97	36	26	31	18	1	0	31	2	592	62	11%



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Hole_ld	Depth From	Depth To	Be	CeO ₂	Dy ₂ O ₃	Er ₂ O ₃	Eu ₂ O ₃	Gd_2O_3	Ho₂O₃	La ₂ O ₃	Li	Lu ₂ O ₃	Nd_2O_3	Ni	Pr ₆ O ₁₁	Sc ₂ O ₃	Sm ₂ O ₃	Tb ₂ O ₃	Tm₂O₃	Y_2O_3	Yb ₂ O ₃	TREO ppm	HREO ppm	HREO/ TREO
22DAC026	20	24	1	279	6	2	3	9	1	115	8.00	0	79	20	23	21	14		0	25	2	581	50	
22DAC071	48.00	52.00	3	246	11	6	3	14	2	82	78.50	1	84	38	23	25	15	2	1	59	5	580	105	18%
22DAC047	16	20	1	206	4	2	3	7	1	172	27.00	0	99	94	32	18	14	1	0	19	2	579	38	7%
22DAC059	44.00	48.00	1.5	271	7	3	4	12	1	78	22.00	0		34	25	28	17		0	30	2	575	60	10%
22DAC078	8	12	-0.5	242	10	4	5	17	2	93	2.00	0	103	6	24	9	21		0	37	3	572	79	14%
22DAC071	52.00	56.00	3.5	246	11	6	2	12	2	84	98.00	1	83	48	23	21	15	_	1	58	5	572	100	17%
22DAC062	12.00	16.00	9.5	239	8	4	4	14	1	84	19.50	0	106	136	28	15	19	2	0	44	3	571	81	14%
22DAC095	32	36	1.5	265	6	3	4	10	1	97	10.50	0	94	28	26	18	17	1	0	24	2	571	53	9%
22DAC066	8.00	12.00	4.5	461	4	3	1	5	1	16	55.00	0	22	182	6	18	5	-	0	24	3	569	42	7%
22DAC071	60.00	64.00	3.5	236	11	6	2	13	2	86	72.50	1	82	30	23	21	15	2	1	62	5	569	106	19%
22DAC059	36.00	40.00	1	194	8	4	5	13	1	87	21.50	0	129	48	33	25	21	1	1	39	3	567	77	14%
22DAC047	32	35	1	254	5	2	2	7	1	122	40.00	0	73	106	21	40	11	1	0	22	3	566	44	8%
22DAC072	40.00	42.00	3.5	252	11	6	3	14	2	80	82.50	1	78	48	22	18	15	2	1	55	5	564	98	17%
22DAC026	28	32	1	282	5	2	3	9	1	91	5.00	0	83	12	23	28	14	1	0	18	1	560	39	7%
22DAC073	80.00	81.00	3.5	231	12	7	2	13	2	80	84.00	1	76	38	21	25	14	2	1	67	6	559	113	20%
22DAC073	72.00	76.00	3.5	232	11	6	2	13	2	82	105.00	1	81	44	22	18	15	2	1	63	5	557	107	19%
22DAC074	48.00	52.00	3.5	231	12	6	2	13	2	82	83.00	1	79	48	22	21	15	2	1	63	6	557	107	19%
22DAC073	64.00	68.00	3.5	231	11	6	2	13	2	78	106.00	1	75	36	21	25	14	2	1	61	6	549	105	19%
22DAC062	4.00	8.00	1.5	246	5	2	3	9	1	108	20.00	0	91	48	25	15	14	1	0	21	1	545	45	8%
22DAC071	72.00	76.00	4	226	11	6	2	12	2	84	75.50	1	78	32	22	18	15	2	1	59	6	544	101	19%
22DAC073	76.00	80.00	3.5	233	10	5	2	11	2	84	103.00	1	76	34	21	18	14	2	1	52	5	537	90	17%
22DAC095	24	28	1	231	9	3	4	13	1	88	30.50	0	89	22	24	12	17	2	0	37	3	533	73	14%
22DAC071	68.00	72.00	4	230	9	5	2	11	2	93	70.00	1	75	32	22	15	13	2	1	47	4	530	83	16%
22DAC070	16.00	20.00	2	131	12	6	5	17	2	94	32.00	1	116	96	29	18	22	2	1	65	6	529	118	22%
22DAC071	44.00	48.00	3	201	11	8	2	12	2	72	75.00	1	72	34	19	25	13	2	1	78	7	527	125	24%
22DAC071	64.00	68.00	3.5	221	10	5	2	11	2	86	65.00	1	74	32	21	18	13	2	1	55	5	526	93	18%
22DAC074	36.00	40.00	3.5	212	12	7	2	13	2	72	75.00	1	70	34	19	18	14	2	1	72	7	526	119	23%
22DAC009	24.00	25.00	1.5	254	2	1	2	4	0	126	6.00	0	62	18	20	34	8	0	0	11	1	525	22	4%
22DAC074	28.00	32.00	3	230	10	5	2	12	2	74	70.00	1	73	34	20	18	14	2	1	51	5	520	90	17%
22DAC074	40.00	44.00	3.5	219	10	6	2	12	2	74	84.50	1	70	38	20	21	13	2	1	55	5	511	94	18%
22DAC016	32	35	1.5	221	5	2	3	9		82	13.50	0	99	38	25	28	17		0	15	1	510	38	7%
22DAC039	20	24	1.5	244	3	1	1	4	0	142	12.00	0	46	58	18	25	6	0	0	12	1	504	24	5%
22DAC075	36.00	40.00	1.5	199	8	3	4	12	1	77	14.00	0	87	58	21	34	18	2	0	34	3	503	68	13%
22DAC096	0	4	2	182	9	4	4	14	2	85	29.00	0	93	62	24	15	17	2	1	45	3	500	83	17%



APPENDIX 2. AIR CORE HOLE COLLAR COORDINATES

Tenement	Prospect	Hole_ld	Drill_Type	Mapsheet_ Name	Orig_RL	Orig_GridID	MGA_East	MGA_Nort	MGA_GridID	urveyMetho	Total_Dep th m	Aziº	Dipº	Hole diameter	Elevation
E63/2046	Dundas	22DAC001	AC	Norseman	450	MGA94_51	432300	6421850	MGA94_51	Averaged Po	41	90	-60	110 cm	450m
E63/2046	Dundas	22DAC002	AC	Norseman	450	MGA94_51	432400	6421850	MGA94_51	Averaged Po	42	90	-60	110 cm	450m
E63/2046	Dundas	22DAC003	AC	Norseman	450	MGA94_51	432500	6421850	MGA94_51	Averaged Po	28	90	-60	110 cm	450m
E63/2046	Dundas	22DAC004	AC	Norseman	450	MGA94_51	432600	6421850	MGA94_51	Averaged Po	14	90	-60	110 cm	450m
E63/2046	Dundas	22DAC005	AC	Norseman	450	MGA94_51	432700	6421850	MGA94_51	Averaged Po	22	90	-60	110 cm	450m
E63/2046	Dundas	22DAC006	AC	Norseman	450	MGA94_51	432800	6421850	MGA94_51	Averaged Po	28	90	-60	110 cm	450m
E63/2046	Dundas	22DAC007	AC	Norseman	450	MGA94_51	433100	6421850	MGA94_51	Averaged Po	24	90	-60	110 cm	450m
E63/2046	Dundas	22DAC008	AC	Norseman	450	MGA94_51	433200	6421850	MGA94_51	Averaged Po	20	90	-60	110 cm	450m
E63/2046	Dundas	22DAC009	AC	Norseman	450	MGA94_51	433300	6421850	MGA94_51	Averaged Po	25	90	-60	110 cm	450m
E63/2046	Dundas	22DAC010	AC	Norseman	450	MGA94_51	433400	6421850	MGA94_51	Averaged Po	14	90	-60	110 cm	450m
E63/2046	Dundas	22DAC011	AC	Norseman	450	MGA94_51	433500	6421850	MGA94_51	Averaged Po	24	90	-60	110 cm	450m
E63/2046	Dundas	22DAC012	AC	Norseman	450	MGA94_51	433600	6421850	MGA94_51	Averaged Po	9	90	-60	110 cm	450m
E63/2046	Dundas	22DAC013	AC	Norseman	450	MGA94_51	433000	6421050	MGA94_51	Averaged Po	15	90	-60	110 cm	450m
E63/2046	Dundas	22DAC014	AC	Norseman	450	MGA94_51	433100	6421050	MGA94_51	Averaged Po	6	90	-60	110 cm	450m
E63/2046	Dundas	22DAC015	AC	Norseman	450	MGA94_51	433200	6421050	MGA94_51	Averaged Po	10	90	-60	110 cm	450m
E63/2046	Dundas	22DAC016	AC	Norseman	450	MGA94_51	433300	6421050	MGA94_51	Averaged Po	35	90	-60	110 cm	450m
E63/2046	Dundas	22DAC017	AC	Norseman	450	MGA94_51	433400	6421050	MGA94_51	Averaged Po	10	90	-60	110 cm	450m
E63/2046	Dundas	22DAC018	AC	Norseman	450	MGA94_51	433500	6421050	MGA94_51	Averaged Po	16	90	-60	110 cm	450m
E63/2046	Dundas	22DAC019	AC	Norseman	450	MGA94_51	432300	6420650	MGA94_51	Averaged Po	34	90	-60	110 cm	450m
E63/2046	Dundas	22DAC020	AC	Norseman	450	MGA94_51	432400	6420650	MGA94_51	Averaged Po	42	90	-60	110 cm	450m
E63/2046	Dundas	22DAC021	AC	Norseman	450	MGA94_51	432500	6420650	MGA94_51	Averaged Po	32	90	-60	110 cm	450m
E63/2046	Dundas	22DAC022	AC	Norseman	450	MGA94_51	432600	6420650	MGA94_51	Averaged Po	28	90	-60	110 cm	450m
E63/2046	Dundas	22DAC023	AC	Norseman	450	MGA94_51	432700	6420650	MGA94_51	Averaged Po	31	90	-60	110 cm	450m
E63/2046	Dundas	22DAC024	AC	Norseman	450	MGA94_51	432800	6420650	MGA94_51	Averaged Po	24	90	-60	110 cm	450m
E63/2046	Dundas	22DAC025	AC	Norseman	450	MGA94_51	432850	6420650	MGA94_51	Averaged Po	35	90	-60	110 cm	450m
E63/2046	Dundas	22DAC026	AC	Norseman	450	MGA94_51	432900	6420650	MGA94_51	Averaged Po	35	90	-60	110 cm	450m
E63/2046	Dundas	22DAC027	AC	Norseman	450	MGA94_51	432950	6420650	MGA94_51	Averaged Po	29	90	-60	110 cm	450m
E63/2046	Dundas	22DAC028	AC	Norseman	450	MGA94_51	433000	6420650	MGA94_51	Averaged Po	31	90	-60	110 cm	450m
E63/2046	Dundas	22DAC029	AC	Norseman	450	MGA94_51	433050	6420650	MGA94_51	Averaged Po	14	90	-60	110 cm	450m
E63/2046	Dundas	22DAC030	AC	Norseman	450	MGA94_51	433100	6420650	MGA94_51	Averaged Po	4	90	-60	110 cm	450m
E63/2046	Dundas	22DAC031	AC	Norseman	450	MGA94_51	433150	6420650	MGA94_51	Averaged Po	3	90	-60	110 cm	450m
E63/2046	Dundas	22DAC032	AC	Norseman	450	MGA94_51	433200	6420650	MGA94_51	Averaged Po	2	90	-60	110 cm	450m
E63/2046	Dundas	22DAC033	AC	Norseman	450	MGA94_51	433300	6420650	MGA94_51	Averaged Po	3	90	-60	110 cm	450m



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Tenement	Prospect	Hole_ld	Drill_Type	Mapsheet_ Name	Orig_RL	Orig_GridID	MGA_East	MGA_Nort	MGA_GridID	urveyMetho	Total_Dep	Aziº	Dipº	Hole diameter	Elevation
E63/2046	Dundas	22DAC034	AC	Norseman	450	MGA94_51	433400	6420650	MGA94_51	Averaged Po	3	90	-60	110 cm	450m
E63/2046	Dundas	22DAC035	AC	Norseman	450	MGA94_51	433500	6420650	MGA94_51	Averaged Po	14	90	-60	110 cm	450m
E63/2046	Dundas	22DAC036	AC	Norseman	450	MGA94_51	432800	6420230	MGA94_51	Averaged Po	29	90	-60	110 cm	450m
E63/2046	Dundas	22DAC037	AC	Norseman	450	MGA94_51	432900	6420230	MGA94_51	Averaged Po	17	90	-60	110 cm	450m
E63/2046	Dundas	22DAC038	AC	Norseman	450	MGA94_51	433000	6420230	MGA94_51	Averaged Po	21	90	-60	110 cm	450m
E63/2046	Dundas	22DAC039	AC	Norseman	450	MGA94_51	433050	6420230	MGA94_51	Averaged Po	27	90	-60	110 cm	450m
E63/2046	Dundas	22DAC040	AC	Norseman	450	MGA94_51	433100	6420230	MGA94_51	Averaged Po	23	90	-60	110 cm	450m
E63/2046	Dundas	22DAC041	AC	Norseman	450	MGA94_51	433150	6420230	MGA94_51	Averaged Po	38	90	-60	110 cm	450m
E63/2046	Dundas	22DAC042	AC	Norseman	450	MGA94_51	433200	6420230	MGA94_51	Averaged Po	24	90	-60	110 cm	450m
E63/2046	Dundas	22DAC043	AC	Norseman	450	MGA94_51	433250	6420230	MGA94_51	Averaged Po	4	90	-60	110 cm	450m
E63/2046	Dundas	22DAC044	AC	Norseman	450	MGA94_51	433300	6420230	MGA94_51	Averaged Po	5	90	-60	110 cm	450m
E63/2046	Dundas	22DAC045	AC	Norseman	450	MGA94_51	433400	6420230	MGA94_51	Averaged Po	27	90	-60	110 cm	450m
E63/2046	Dundas	22DAC046	AC	Norseman	450	MGA94_51	433500	6420230	MGA94_51	Averaged Po	11	90	-60	110 cm	450m
E63/2046	Dundas	22DAC047	AC	Norseman	450	MGA94_51	432900	6420060	MGA94_51	Averaged Po	35	90	-60	110 cm	450m
E63/2047	Dundas	22DAC047a	AC	Norseman	451	MGA94_52	432950	6420060	MGA94_51	Averaged Po	34	90	-60	110 cm	450m
E63/2046	Dundas	22DAC048	AC	Norseman	450	MGA94_51	433000	6420060	MGA94_51	Averaged Po	26	90	-60	110 cm	450m
E63/2046	Dundas	22DAC049	AC	Norseman	450	MGA94_51	433100	6420060	MGA94_51	Averaged Po	20	90	-60	110 cm	450m
E63/2046	Dundas	22DAC050	AC	Norseman	450	MGA94_51	433200	6420060	MGA94_51	Averaged Po	16	90	-60	110 cm	450m
E63/2046	Dundas	22DAC051	AC	Norseman	450	MGA94_51	433250	6420060	MGA94_51	Averaged Po	19	90	-60	110 cm	450m
E63/2046	Dundas	22DAC052	AC	Norseman	450	MGA94_51	433300	6420060	MGA94_51	Averaged Po	31	90	-60	110 cm	450m
E63/2046	Dundas	22DAC053	AC	Norseman	450	MGA94_51	433400	6420060	MGA94_51	Averaged Po	27	90	-60	110 cm	450m
E63/2046	Dundas	22DAC054	AC	Norseman	450	MGA94_51	433500	6420060	MGA94_51	Averaged Po	5	90	-60	110 cm	450m
E63/2046	Dundas	22DAC055	AC	Norseman	450	MGA94_51	433100	6419660	MGA94_51	Averaged Po	46	90	-60	110 cm	450m
E63/2046	Dundas	22DAC056	AC	Norseman	450	MGA94_51	433200	6419660	MGA94_51	Averaged Po	46	90	-60	110 cm	450m
E63/2046	Dundas	22DAC057	AC	Norseman	450	MGA94_51	433300	6419660	MGA94_51	Averaged Po	42	90	-60	110 cm	450m
E63/2046	Dundas	22DAC058	AC	Norseman	450	MGA94_51	433400	6419660	MGA94_51	Averaged Po	63	90	-60	110 cm	450m
E63/2046	Dundas	22DAC059	AC	Norseman	450	MGA94_51	433500	6419660	MGA94_51	Averaged Po	46	90	-60	110 cm	450m
E63/2046	Dundas	22DAC060	AC	Norseman	450	MGA94_51	433600	6419660	MGA94_51	Averaged Po	33	90	-60	110 cm	450m
E63/2046	Dundas	22DAC061A	AC	Norseman	450	MGA94_51	433300	6418850	MGA94_51	Averaged Po	18	90	-60	110 cm	450m
E63/2047	Dundas	22DAC061B	AC	Norseman			433300	6418850	MGA94_51	Averaged Po	30	90	-60	110 cm	450m
E63/2046	Dundas	22DAC061	AC	Norseman	450	MGA94_51	433400	6418850	MGA94_51	Averaged Po	26	90	-60	110 cm	450m
E63/2046	Dundas	22DAC062	AC	Norseman	450	MGA94_51	433500	6418850	MGA94_51	Averaged Po	35	90	-60	110 cm	450m
E63/2046	Dundas	22DAC063	AC	Norseman	450	MGA94_51	433600	6418850	MGA94_51	Averaged Po	48	90	-60	110 cm	450m



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Tonomont	Broomoot	Uolo Id	Drill_Type	Mapsheet_	Oria DI	Oria CridID	MCA Foot	MGA_Nort	MGA_GridID	umayMatha	Total_Dep			Hole	
Tenement	Prospect	Hole_Id	Dill_Type	Name	Orig_RL	Orig_GridID	WGA_East	h	WGA_GHaiD	urveyMetho	th m	Aziº	Dipº	diameter	Elevation
E63/2046	Dundas	22DAC064	AC	Norseman	450	MGA94_51	433700	6418850	MGA94_51	Averaged Po	40	90	-60	110 cm	450m
E63/2046	Dundas	22DAC065	AC	Norseman	450	MGA94_51	433800	6418850	MGA94_51	Averaged Po	41	90	-60	110 cm	450m
E63/2046	Dundas	22DAC066	AC	Norseman	450	MGA94_51	433900	6418850	MGA94_51	Averaged Po	32	90	-60	110 cm	450m
E63/2046	Dundas	22DAC067	AC	Norseman	450	MGA94_51	433450	6418600	MGA94_51	Averaged Po	31	90	-60	110 cm	450m
E63/2046	Dundas	22DAC068	AC	Norseman	450	MGA94_51	433550	6418600	MGA94_51	Averaged Po	41	90	-60	110 cm	450m
E63/2046	Dundas	22DAC069	AC	Norseman	450	MGA94_51	433650	6418600	MGA94_51	Averaged Po	31	90	-60	110 cm	450m
E63/2046	Dundas	22DAC070	AC	Norseman	450	MGA94_51	433750	6418600	MGA94_51	Averaged Po	29	90	-60	110 cm	450m
E63/2046	Dundas	22DAC071	AC	Norseman	450	MGA94_51	433500	6418000	MGA94_51	Averaged Po	84	90	-60	110 cm	450m
E63/2046	Dundas	22DAC072	AC	Norseman	450	MGA94_51	433600	6418000	MGA94_51	Averaged Po	42	90	-60	110 cm	450m
E63/2046	Dundas	22DAC073	AC	Norseman	450	MGA94_51	433700	6418000	MGA94_51	Averaged Po	81	90	-60	110 cm	450m
E63/2046	Dundas	22DAC074	AC	Norseman	450	MGA94_51	433800	6418000	MGA94_51	Averaged Po	63	90	-60	110 cm	450m
E63/2046	Dundas	22DAC075	AC	Norseman	450	MGA94_51	434050	6420460	MGA94_51	Averaged Po	82	90	-60	110 cm	450m
E63/2046	Dundas	22DAC076	AC	Norseman	450	MGA94_51	434150	6420460	MGA94_51	Averaged Po	35	90	-60	110 cm	450m
E63/2046	Dundas	22DAC077	AC	Norseman	450	MGA94_51	434250	6420460	MGA94_51	Averaged Po	30	90	-60	110 cm	450m
E63/2046	Dundas	22DAC078	AC	Norseman	450	MGA94_51	434100	6419840	MGA94_51	Averaged Po	25	90	-60	110 cm	450m
E63/2046	Dundas	22DAC079	AC	Norseman	450	MGA94_51	434200	6419840	MGA94_51	Averaged Po	48	90	-60	110 cm	450m
E63/2046	Dundas	22DAC080	AC	Norseman	450	MGA94_51	434300	6419840	MGA94_51	Averaged Po	33	90	-60	110 cm	450m
E63/2046	Dundas	22DAC081	AC	Norseman	450	MGA94_51	434400	6419840	MGA94_51	Averaged Po	27	90	-60	110 cm	450m
E63/2046	Dundas	22DAC082	AC	Norseman	450	MGA94_51	434500	6419840	MGA94_51	Averaged Po	16	90	-60	110 cm	450m
E63/2046	Dundas	22DAC083	AC	Norseman	450	MGA94_51	434600	6419840	MGA94_51	Averaged Po	7	90	-60	110 cm	450m
E63/2046	Dundas	22DAC084	AC	Norseman	450	MGA94_51	434400	6419350	MGA94_51	Averaged Po	9	90	-60	110 cm	450m
E63/2046	Dundas	22DAC085	AC	Norseman	450	MGA94_51	434500	6419350	MGA94_51	Averaged Po	7	90	-60	110 cm	450m
E63/2046	Dundas	22DAC086	AC	Norseman	450	MGA94_51	434600	6419350	MGA94_51	Averaged Po	28	90	-60	110 cm	450m
E63/2046	Dundas	22DAC087	AC	Norseman	450	MGA94_51	434700	6419350	MGA94_51	Averaged Po	44	90	-60	110 cm	450m
E63/2046	Dundas	22DAC088	AC	Norseman	450	MGA94_51	434400	6418750	MGA94_51	Averaged Po	10	90	-60	110 cm	450m
E63/2046	Dundas	22DAC089	AC	Norseman	450	MGA94_51	434500	6418750	MGA94_51	Averaged Po	18	90	-60	110 cm	450m
E63/2047	Dundas	22DAC089a	AC	Norseman			434550	6418750	MGA94_51	Averaged Po	26	90	-60	110 cm	450m
E63/2046	Dundas	22DAC090	AC	Norseman	450	MGA94_51	434600	6418750	MGA94_51	Averaged Po	26	90	-60	110 cm	450m
E63/2046	Dundas	22DAC091	AC	Norseman	450	MGA94_51	434700	6418750	MGA94_51	Averaged Po	43	90	-60	110 cm	450m
E63/2046	Dundas	22DAC092	AC	Norseman	450	MGA94_51	434800	6418750	MGA94_51	Averaged Po	32	90	-60	110 cm	450m
E63/2046	Dundas	22DAC093	AC	Norseman	450	MGA94_51	434900	6418750	MGA94_51	Averaged Po	47	90	-60	110 cm	450m
E63/2046	Dundas	22DAC094	AC	Norseman	450	MGA94 51	434450	6418400	MGA94_51	Averaged Po	26	90	-60	110 cm	450m
E63/2046	Dundas	22DAC095	AC	Norseman	450	MGA94 51	434550	6418400	MGA94_51	Averaged Po	37	90	-60	110 cm	450m
E63/2046	Dundas	22DAC096	AC	Norseman	450	MGA94 51	434650	6418400	MGA94 51	Averaged Po	35	90	-60	110 cm	450m
E63/2046	Dundas	22DAC097	AC	Norseman	450	MGA94 51	434750	6418400	MGA94 51	Averaged Po	49	90	-60	110 cm	450m
E63/2046	Dundas	22DAC098	AC	Norseman	450	MGA94 51	434850	6418400	MGA94 51	Averaged Po	65	90	-60	110 cm	450m
E63/2046	Dundas	22DAC099	AC	Norseman	450	MGA94 51	434950	6418400	MGA94 51	Averaged Po	81	90	-60	110 cm	450m



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JORC Code, 2012 Edition - Table 1

Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g., cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling. Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.	 Catalina Resources completed 105 air core drill holes for 2909m at its Dundas prospect, Norseman, WA. Drilling is located within Catalina's E63/2046, during Nov & Dec 2022. Air core sampling was undertaken at 1-m intervals using a Meztke Static Cyclone. Most 1-meter samples were dry and weighed between 1.5 and 3 kg. Occasional ground water intersected at the bottom of holes caused some samples to be wet. 1-meter sample piles from the cyclone were laid out in orderly rows on the ground. Using a hand-held trowel, 4m composite samples were collected from the one-meter piles. This compositing was aimed to reduce assaying costs. These composite samples weighed between 2 and 3 kg. For any anomalous 4m composite sample assays, the corresponding one-meter samples will be collected and assayed (fire assay) in the new year. Quality control of the assaying comprised the collection of a duplicate sample every second hole, along with the regular insertion of industry (OREAS) standards (certified reference material) every other hole. Samples were sent to Bureau Veritas labs in Kalgoorlie. Samples will be pulverized so that 75% of the sample passes 75µ. A 30-g charge from each of the pulp will then be



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Criteria	JORC Code explanation	Commentary
		digested via aqua regia acid and fire assay. Only Au will be assayed in Kalgoorlie via BV code FA001, fire assay. • Pulps will then be forwarded to Bureau Veritas Labs in Cannington for analysis of 48 elements (incl REEs, Be and Li) via a mixed acid digest. BV Code MA102.
Drilling techniques	Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	 The drilling contractor was Gyro Drilling from Kalgoorlie. Gyro uses 3m drill rods. Drilling to blade refusal (rock too hard to penetrate); Hole diameter 85mm / 3.5". Air core drilling uses a three-bladed steel or tungsten drill bit to penetrate the weathered layer of loose soil and rock fragments. The drill rods are hollow and feature an inner tube with an outer barrel (like RC drilling). Air core drilling uses small compressors (750 CFM/250 PSI) to drill holes into the weathered layer of loose soil and fragments of rock. After drilling is complete, an injection of compressed air is unleashed into the space between the inner tube and the drill rods inside wall, which flushes the cuttings up and out of the drill hole through the rod's inner tube, causing less chance of cross-contamination. Air core drill rigs are lighter in weight than other rigs, meaning they're quicker and more maneuverable in the bush. Gyro used an Air 750 CFM / 250 PSI Sullair Compressor with additional Air Booster Support 750 CFM / 250PSI.
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed. Measures taken to maximise sample	Representative air core samples collected as 2- meter intervals, with corresponding chips placed into chip trays and kept for reference at Catalina's facilities.



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Criteria	JORC Code explanation	Commentary
	recovery and ensure representative nature of the samples. Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse grained material.	 Most samples were dry and sample recovery was very good. Catalina does not anticipate any sample bias from loss/gain of material from cyclone.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography. The total length and percentage of the relevant intersections logged.	 All air core samples were lithologically logged using standard industry logging software on a notebook computer. Carbonate alteration was logged using hydrochloric acid and magnetism recorded using a hand-held magnetic pen. Logging is qualitative in nature. Drill sample piles and chip trays have been photographed. All geological information noted above has been completed by a competent person as recognized by JORC.
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken. If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry. For all sample types, the nature, quality and appropriateness of the sample preparation technique. Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples. Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.	 Air core sampling was undertaken on 1m intervals using a Meztke Static Cone splitter. Most 1-meter samples were dry and weighed between 2 and 3 kg. Samples from the cyclone were laid out in orderly rows on the ground. Using a hand-held trowel, 4m composite samples were collected from the one-meter piles. These composite samples weighed between 2 and 3 kg. For any anomalous 4m composite sample assays, the corresponding one-meter samples are also collected and assayed. Quality control of the assaying comprised the collection of a duplicate sample every hole, along



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Criteria	JORC Code explanation	Commentary
	Whether sample sizes are appropriate to the grain size of the material being sampled.	with the regular insertion of industry (OREAS) standards (certified reference material) every hole. • Samples were delivered to Bureau Veritas labs in Kalgoorlie by Catalina's field personnel. • Samples were pulverized so that 75% of the sample passes 75µ. • Samples pulps were digested via aqua regia acid. Gold was assayed via BV method FA001, fire assay • Pulps were then forwarded to Bureau Veritas Labs in Cannington for analysis of 48 elements via BV code MA102.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. Nature of quality control procedures adopted (e.g., standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e., lack of bias) and precision have been established.	 All assaying was completed by Bureau Veritas Labs. 4m Composite samples were assayed by Aqua Regia (AR) with ICP-MS (partial digest) BV method FA001. Sample detection is 100 ppb Au. REE, Li and pathfinders were assayed by BV method MA102 (Mixed Acid digestion). BV indicate the mixed acid digestion is an almost complete dissolution method. After collection, anomalous one-meter samples will be assayed at BV labs, Perth. Composite samples were dissolved via a mixed acid (4 acid) digest and read by the ICP MS instrument. Standards were industry CRMs from OREAS which included low-grade and average- grade. The methods are considered appropriate for this style of mineralization expected. No density data available. BV labs routinely re-assay anomalous assays (greater than 0.3 g/t Au) as part of their normal QAQC procedures.



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Criteria	JORC Code explanation	Commentary
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel. The use of twinned holes. Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. Discuss any adjustment to assay data.	 No verification of significant intersections undertaken by independent personnel, only the VG geologist. Validation of 4m composite assay data will be undertaken to compare duplicate assays, standard assays. Comparison of assaying between the composite samples (fire assay digest) and the 1-meter samples (fire assay digest) was made. Comparison of assaying between the composite samples (mixed acid digest) and the 1-meter samples (mixed acid digest) and the 1-meter samples (mixed acid digest) was made. Data is entered into a software program in a desk top computer for eventual download into the company database.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. Specification of the grid system used. Quality and adequacy of topographic control.	 All air core drill hole coordinates are in GDA94 Zone 51 (Appendix 2). All air core holes were located by handheld GPS with an accuracy of +/- 3 m. There is no detailed documentation regarding the accuracy of the topographic control. No elevation values (Z) were recorded for collars. An elevation of 450 mRL was assigned by VG. There were no down-hole surveys completed as air core drill holes were not drilled deep enough to warrant downhole surveying.
Data spacing and distribution	Data spacing for reporting of Exploration Results. Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	 Air core drilling was on a variable line spacing (160m to 500m) and 100m between drill holes. Given the first pass nature of the exploration programs, the spacing of the exploration drilling is appropriate for understanding the exploration potential and the identification of structural controls on the mineralisation.



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Criteria	JORC Code explanation	Commentary
	Whether sample compositing has been applied.	 Four- meter sample compositing has been applied.
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	 The relationship between drill orientation and the mineralised structures is not known at this stage as the prospects are covered by a 3-12m blanket of transported cover. It is concluded from aerial magnetics that the mineralisation trends 000. Dips are unknown as the area is covered by a 3m – 12m blanket of transported cover. Azimuths and dips of air core drilling was aimed to intersect the strike of the rocks at right angles. Downhole widths of mineralisation are not known with assays not yet received.
Sample security	The measures taken to ensure sample security.	 All samples packaged and managed by Catalina personnel up to and including the delivery of all samples to BV labs.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	 No sampling techniques or data have been independently audited.

Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to	 The Dundas Project is within E63/2046. They form part of a broader tenement package of four exploration tenements located in the Dundas Goldfields in the Norseman region of Western Australia. The project area was culturally surveyed and cleared in Sept 2022 by the Ngadju Native Title Aboriginal Corporation.
	operate in the area.	



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Criteria	JORC Code explanation	Commentary
		 There are no registered cultural heritage sites within the area.
		 E63/2046 and E63/2048 are held 100% by Catalina Resources. All tenements are secured by the DMIRS (WA Government).
		 E63/2046 and E63/2048 were granted in 2021. They are in a state of good standing and have no impediments.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	 Only very limited historical exploration has been carried out in the area due to the thin blanket (usually 5 – 20m) of transported cover. In E63/2048, one km spaced auger soil traverses undertaken by AngloGold Ashanti Australia (AngloGold) were completed. A RAB/RC drilling program by Pan Australian Resources during the 1990's identified the presence of gold mineralisation hosted by mafic rocks in E63/2046. Reported intersections include: T4RC032 2m @ 3.5g/t Au from 23m T4RC042 1m @ 2.1g/t Au from 87m
		 The mineralization discussed above remains open, and the associated Au and Cu soil geochemistry (AngloGold's data) suggests the mineralization is much more extensive than indicated by past drilling. Several large and robust gold in soil auger geochemical anomalies, up to 6 kms in length, are spatially associated with the interpreted BLFZ (Boulder Lefroy Fault Zone) in E63/2048 and represents a high priority for targeting by Catalina.
Geology	Deposit type, geological setting and	The Dundas Project forms part of an underexplored



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Criteria	JORC Code explanation	Commentary
	style of mineralisation.	green fields region in the Albany Fraser Belt. In 2005, the discovery of the multimillion-ounce Tropicana gold deposit in 2005, 330 kms east of Kalgoorlie in the Albany Fraser Belt, initiated a reassessment of the prospectivity of the province. • A program of geophysical surveys and geoscientific work, including age dating of rocks, undertaken by the Geological Survey of Western Australia, during 2006-2010, has subsequently shown the Albany Fraser belt to contain reworked Archaean greenstones. • The Project area is now considered to be situated within the inferred SE extensions of the Norseman – Wiluna Belt of the Archaean Yilgarn Craton and comprises a tectonostratigraphic assemblage of mafic, ultramafic and sedimentary dominated units. A major northwest trending fault system transects the tenements and may represent southeast extensions of the prolifically mineralised and regionally continuous Zuleika and Boulder-Lefroy Fault systems. • Greenstone belts are commonly hosts to gold and rare-element pegmatities because they are both products of collisional tectonic processes. Rare element pegmatites form in orogenic hinterlands related to plate convergence. • The pegmatites are products of extreme fractional crystallization of some granites, derived from melting of metasedimentary rocks in continental collision zones. The world class Buldannia Lithium Project (Liontown Resources) is situated just 25 kms northwest of Catalina's tenements, interpreted to be within the Zuleika Shear Zone.
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the	 Appendix 1 (Air core hole assays) lists information material to the understanding of the air core drill holes at the Dundas Projects.



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Criteria	JORC Code explanation	Commentary
	following information for all Material drill holes: easting and northing of the drill hole collar elevation or RL (Reduced Level – elevation above sea level in meters) of the drill hole collar dip and azimuth of the hole down hole length and interception depth hole length. If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	 Appendix 2 (air core collar coordinates) lists information material to the understanding of the air core drill holes at the Dundas Projects. The documentation for drill hole locations is located in the appendices of this announcement and is considered acceptable by VG. Consequently, the use of any data obtained is suitable for presentation and analysis. Given the early stages of the exploration programs, the data quality is acceptable for reporting purposes. Future drilling programs are dependent on the assays received.
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g., cutting of high grades) and cut-off grades are usually Material and should be stated. Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low- grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. The assumptions used for any reporting of metal equivalent values should be clearly stated.	 NA. Drilling sample assay results for most of 48 elements are tabulated in appendix 1. Samples were collected as 4m composite samples from the drill rig. Composite samples are collected purely as a way to reduce costs.



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Criteria	JORC Code explanation	Commentary
Relationship between mineralisation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results. If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g., 'down hole length, true width not known').	 NA Exploration has not determined the geometry and extent of any mineralization discussed in this announcement. Further drilling is required to ascertain the geometry of any intersection.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Diagrams showing historical drilling data, current drill hole collar plans, downhole air core assaying, are used in text of this announcement.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	 Exploration results that may create biased reporting has been omitted from these documents. Appendix 1 – Air core downhole assays. Appendix 2 – Air core drill holes collar coordinates.
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	No additional exploration data has been reported. All holes were geologically logged but are not included in this announcement as they were not considered material.



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Criteria	JORC Code explanation	Commentary
Further work	The nature and scale of planned further work (e.g., tests for lateral extensions or depth extensions or large-scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	 Auger drilling of large historical auger geochemistry anomalies is planned to commence within E63/2048 later in 2023. Further drilling (including RC drilling) in E63/2046 is being planned. A new CMP has been submitted to the DBCA detailing Catalina's plans for work in the other tenements. Regional detailed aerial magnetic surveys may commence over the priority target areas, as identified by Catalina.